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THE 8638

IRON MANUAL;

WITH TABLES,

SHOWING THE SIZE AND WEIGHT OF

IRON, STEEL, TIN PLATES, &c.

Entered, according to Act of Congress, in the year 1868, by

HENRY M. JOHNSON,

In the Clerk's Office of the District Court of the District of Mass.

BOSTON, MASS.

1868.

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HENRY M. JOHNSON.
IRON, STEEL, AND METALS,

36 India Street.

BOSTON, MASS.

Best Refined Iron, for Shafting, Turning,
and Smith's Purposes.

Best Refined Angle, Tee, and Channel Iron.

Bolt and Spike Iron.

Pail, Tub, and Trunk Iron.

Hoop, Band, and Scroll Iron.

Boiler Plates, Tank and Sheet Iron.

Oval, Half-Oval, and Half-Round Iron.

Norway and Swedes Iron, Rods and Shapes.

Norway Nail Rods and Plates. Extra quality.

Steel of all descriptions.

IRON,

ON account of its abundance, working qualities, and tenacity, is probably the most useful and valuable of metals.

In its primitive position it is commingled with the earth's strata in bountiful profusion. It is found in various combinations and conditions in every formation, and it is a constituent element of both animals and vegetables.

THE ORES.

The ores of iron are found in profuse abundance in every latitude. Imbedded in, or stratified with every formation, they occur both crystallized, massive, and arenaceous; lying deep in strata of vast extent, filling veins and faults in other rocks, and scattered over the surface of the ground. Sometimes, but rarely, found native; usually as oxides, sulphurets, or carbonates, more or less mingled with other substances.

CONVERSION OF CRUDE INTO MALLEABLE IRON.

The conversion of the carbonized crude iron, obtained from the blast furnace, into malleable or

wrought iron, is effected by several operations of an oxidizing character, in which it is sought to separate, in the gaseous state, the carbon contained in the iron by combining it with oxygen, whilst the other metals, alloyed with the iron and the phosphorus, pass into the slag.

The iron produced in the smelting furnace may be divided into two kinds,—that reduced by charcoal, and that reduced by coke, or raw coal. When charcoal iron has to be converted by charcoal,—as in Sweden,—it is decarbonized in the charcoal refinery, with or without an intervening process. Where coal can be obtained, however, it is now usually converted by the process of puddling. Pig iron, produced by coke or coal, is converted into malleable iron either by decarbonization in the refinery, or oxidizing hearth, and subsequent puddling, or it is converted at once in the puddling furnace by the process of boiling,—which is equally effective, and is now more generally practised.

The crude pig iron is assorted according to the degree and uniformity of its carbonization, and classed as numbers 1, 2, 3, &c.; No. 1 being most highly carbonized, No. 2 less so, and so on to No. 4, which contains much more oxygen than the others. The carbon combined with iron gives it fusibility and fluidity, but deprives it of ductility. To render it malleable, and capable of being welded, it must be deprived, as far as possible, of all the extraneous substances which have been mixed with it in the blast furnace, more especially of the carbon.

Prima facie, therefore, it would appear that the highly carbonized pig iron is the most suitable for

casting, whilst that containing least carbon is best adapted for conversion into malleable iron. Hence, in the trade, the crude iron is divided into foundry and forge pigs.

The pigs, however, in which carbon most predominates, and which, as a rule, have been most effectually separated from all other impurities during the process of smelting, are in many respects preferable for the manufacture of wrought iron. Up to this time, however, great practical difficulties have attended the decarbonization of iron containing so much carbon, and the white or forge iron is almost always preferred, measures having been taken for depriving it of the metals and earthy impurities not separated in the blast furnace.

With regard to the process of refining, we may observe that the crude iron is melted in a hollow fire, and partially decarbonized by the action of a blast of air forced over its surface by a fan or blowing engine; the carbon having greater affinity for the oxygen than for the iron, combines with it, and passes off as gaseous carbonic oxide, or carbonic acid. During this process, a portion of the silicium, &c., is fused out, and separated from the iron. It is obvious from the above, that the iron to be refined, being placed in contact with fuel at a high temperature, is liable to be deteriorated by the admixture of sulphur and other impurities of the fuel; and, as the iron is only partially exposed to the action of the blast, the operation is necessarily, under these circumstances, imperfect. From the refinery the metal is run out into large moulds, and is then broken up into what is technically distinguished as *plate metal*.

The process of puddling succeeds that of refining; and in this operation the reverberatory furnace is employed, with the fire separated by a partition or bridge from the hearth, on which is placed the metal to be puddled. By this arrangement the flame is conducted over the surface of the metal, creating an intense heat; though the deleterious portions of the fuel cannot mix with the iron in this furnace, the iron is kept in a state of fusion, whilst the workman, called the "*puddler*," by means of a rake, or rabble, agitates the metal so as to expose, as far as he is able, the whole of the charge to the action of the oxygen passing over it from the fire. By this means the carbon is oxidized, and the metal is gradually reduced to a tough, pasty condition, and subsequently to a granular form, somewhat resembling heaps of boiled rice, with the grains greatly enlarged. In this condition of the furnace the cinders, or earthy impurities, yield to the intense heat, and flow off from the mass over the bottom in a highly fluid state.

The iron, at this stage, is comparatively pure, and quickly becomes capable of agglutination.

The puddler then collects the metallic granules or particles with his rabble, and rolls them together, backwards and forwards, over the furnace bottom, into balls of convenient dimensions (about the size of 13-inch shells), when he removes them from the furnace, to be subjected to the action of the hammer, or mechanical pressure necessary to give the iron homogeneity and fibre.

These processes of refining and puddling have universally been employed till recently; but improve-

ments have rendered it simpler, and the refining process is now very generally abolished.

Shortly after the employment of the puddling process, it was found advantageous to mix a portion of crude iron with the refined plate metal, the expense of the process of refining being saved upon the iron used in the crude state; and, trusting to the decarbonizing effects of the puddling furnace, it was found that the refining process might be altogether dispensed with, if the crude iron containing a portion of oxygen and a very little carbon, was employed. In this single process, it is to be observed, that as all the carbon has to be got rid of in the puddling furnace, the evolution of gas is much more violent, the fluid iron boiling and bubbling energetically during the period of its disengagement; and hence the operation has acquired the popular name of the "boiling" process.

In this operation the pig iron, when melted, is more fluid, — on account of containing a greater proportion of carbon, — than the metal from the refinery, and requires more labor in stirring it about and submitting it to the action of the current of air. The process, moreover, is attended by a greater waste of iron than puddling either plate or crude iron and plate mixed, but not so great a loss as in the two operations of refining and puddling. It must, however, be admitted that the superior fluidity of the iron in the boiling process has a more injurious action on the furnace.

Notwithstanding these objections, the system of boiling, without the intermediate process of refining, has been gaining ground for the last ten years, and

in many places has entirely superseded the use of the refinery.

Recent events have therefore led to the conclusion, that in a short time the refining process will have become a thing of the past.

RUSSIA SHEET IRON

Measures 56 by 23 inches, and is rated by the weight per sheet. The numbers run from 8 to 18 Russian pounds per sheet. Eight Russian pounds equal 7.2 English pounds; 9 = 8.1 lbs.; 10 = 9 lbs.; 11 = 10 lbs.; 12 = 11.2 lbs., &c. 100 Russian pounds equal 90 pounds English.

GALVANIZED IRON,

IRON alloyed superficially with zinc, by plunging the metal, previously well cleaned by friction with dilute acid, into a bath of melted zinc, covered with sal-ammoniac, and stirring it about for some time, produces that which is known as *Galvanized Iron*.

When iron thus treated is exposed to humidity, the zinc is said to become oxidized in consequence of galvanic action. This coating protects the iron beneath from rusting; and hence galvanized iron will retain its whiteness for a long period, under circumstances that would cause ordinary tinned iron to exhibit marks of corrosion.

To Compute the Weight of Cast Metal by the Weight of the Pattern.

When the Pattern is of White Pine.

RULE. — Multiply the weight of the pattern in pounds by the following multiplier, and the product will give the weight of the casting:

Iron, 14; Brass, 15; Lead, 22; Tin, 14; Zinc, 13.5.

When there are Circular Cores or Prints.

Multiply the square of the diameter of the core or print by its length in inches, the product by .0175, and the result is the weight of the pattern of the core or print, to be deducted from the weight of the pattern.

It is customary, in the making of patterns for castings, to allow for shrinkage per lineal foot of pattern:

Iron and Lead, $\frac{1}{8}$ th of an inch, Brass and Zinc, $\frac{3}{16}$ ths, and Tin, $\frac{1}{12}$ th.

Composition for Welding Cast Steel.

Borax, 10 parts; Sal-ammoniac, 1 part. Grind or pound them roughly together; fuse them in a metal pot over a clear fire, continuing the heat until all

spume has disappeared from the surface. When the liquid is clear, pour the composition out to cool and concrete, and grind to a fine powder; then it is ready for use.

To use this composition, the steel to be welded should be raised to a bright yellow heat; then dip it in the welding powder, and again raise it to a like heat as before; it is then ready to be submitted to the hammer.

Shrinkage of Castings.

Iron, small cylinders . . . = $\frac{1}{16}$ inches per foot.

" Pipes = $\frac{1}{8}$ " " "

" Girders, beams, etc. . = $\frac{1}{8}$ in 15 inches.

" Large cylinders, the
contraction of di- } = $\frac{1}{16}$ per foot.
ameter at top . . . }

" Ditto at bottom . . . = $\frac{1}{12}$ per foot.

" Ditto, in length . . . = $\frac{1}{8}$ in 16 inches.

Brass, thin = $\frac{1}{8}$ in 9 inches.

" thick = $\frac{1}{8}$ in 10 inches.

Zinc = $\frac{5}{16}$ in a foot.

Lead = $\frac{5}{16}$ in a foot.

Copper = $\frac{3}{16}$ in a foot.

Bismuth = $\frac{5}{32}$ in a foot.

Fluxes for Soldering or Welding.

Iron Borax.

Tinned Iron Resin.

Copper and Brass Sal-ammoniac.

Zinc Chloride of zinc.

Lead Tallow or resin.

Lead and tin pipes Resin and sweet oil.

Steel — Sal-ammoniac, 1 part; borax 10 parts.
Pound together, and fuse until clear, and, when cool,
reduce to powder.

Babbitt's Anti-Attrition Metal.

Melt 4 lbs. Copper; add, by degrees, 12 lbs. best Banca Tin, 8 lbs. Regulus of Antimony, and 12 lbs. more of Tin. After 4 or 5 lbs. Tin have been added, reduce the heat to a dull red, then add the remainder of the metal as above.

This composition is termed *hardening*; for lining, take 1 lb. of this *hardening*, melt with it 2 lbs. Banca Tin, which produces the lining metal for use. Hence, the proportions for lining metal are 4 lbs. of Copper, 8 of Regulus of Antimony, and 96 of Tin.

To Prevent Iron from Rusting.

Warm it; then rub with white wax; put it again to the fire until the wax has pervaded the entire surface.

Or, immerse tools or bright work in boiled linseed-oil, and allow it to dry upon them.

Weight of Round Rolled Iron, one foot in length.

$1\frac{1}{16}$.010	2	10.616	$5\frac{3}{8}$	76.700
$1\frac{1}{8}$.041	$2\frac{1}{8}$	11.988	$5\frac{1}{2}$	80.304
$1\frac{3}{16}$.094	$2\frac{1}{4}$	13.440	$5\frac{5}{8}$	84.001
$1\frac{1}{4}$.165	$2\frac{3}{8}$	14.975	$5\frac{3}{4}$	87.776
$1\frac{5}{16}$.261	$2\frac{1}{2}$	16.688	$5\frac{7}{8}$	91.634
$1\frac{3}{8}$.373	$2\frac{5}{8}$	18.293	6	95.552
$1\frac{7}{16}$.508	$2\frac{3}{4}$	20.076	$6\frac{1}{4}$	103.704
$1\frac{1}{2}$.663	$2\frac{7}{8}$	21.944	$6\frac{3}{8}$	112.160
$1\frac{9}{16}$.840	3	23.888	$6\frac{3}{4}$	120.960
$1\frac{5}{8}$	1.043	$3\frac{1}{8}$	25.926	7	130.048
$1\frac{11}{16}$	1.255	$3\frac{1}{4}$	28.040	$7\frac{1}{4}$	139.544
$1\frac{3}{4}$	1.493	$3\frac{3}{8}$	30.240	$7\frac{1}{2}$	149.328
$1\frac{13}{16}$	1.752	$3\frac{1}{2}$	32.512	$7\frac{3}{4}$	159.456
$1\frac{7}{8}$	2.032	$3\frac{5}{8}$	34.886	8	169.856
$1\frac{15}{16}$	2.333	$3\frac{3}{4}$	37.332	$8\frac{1}{4}$	180.696
1	2.654	$3\frac{7}{8}$	39.864	$8\frac{3}{8}$	191.808
$1\frac{1}{16}$	2.997	4	42.464	$8\frac{3}{4}$	203.260
$1\frac{1}{8}$	3.360	$4\frac{1}{8}$	45.174	9	215.040
$1\frac{3}{16}$	3.744	$4\frac{1}{4}$	47.952	$9\frac{1}{4}$	227.152
$1\frac{1}{4}$	4.172	$4\frac{3}{8}$	50.815	$9\frac{1}{2}$	239.600
$1\frac{5}{16}$	4.573	$4\frac{1}{2}$	53.760	$9\frac{3}{4}$	252.376
$1\frac{3}{8}$	5.019	$4\frac{5}{8}$	56.788	10	267.008
$1\frac{7}{16}$	5.486	$4\frac{3}{4}$	59.900	$10\frac{1}{4}$	278.924
$1\frac{1}{2}$	5.972	$4\frac{7}{8}$	63.094	$10\frac{1}{2}$	292.688
$1\frac{5}{8}$	7.010	5	66.752	11	321.216
$1\frac{3}{4}$	8.128	$5\frac{1}{8}$	69.731	$11\frac{1}{2}$	351.104
$1\frac{7}{8}$	9.333	$5\frac{1}{4}$	73.172	12	382.208

HENRY M. JOHNSON,
 BAR, HOOP, SHEET, AND ANGLE IRON,
 No. 36 India Street,
 Boston, Mass.

Weight of Square Rolled Iron, one foot in length.

HENRY M. JOHNSON,
NORWAY AND SWEDES IRON, RODS AND SHAPES,
Boston, Mass.
No. 36 India Street,

$\frac{1}{16}$.013	$2\frac{3}{8}$	19.066	$5\frac{3}{4}$	111.756
$\frac{1}{8}$.053	$2\frac{1}{2}$	21.120	$5\frac{7}{8}$	116.671
$\frac{3}{16}$.119	$2\frac{5}{8}$	23.292	6	121.664
$\frac{1}{4}$.211	$2\frac{3}{4}$	25.560	$6\frac{1}{4}$	132.040
$\frac{5}{16}$.330	$2\frac{7}{8}$	27.939	$6\frac{1}{2}$	142.816
$\frac{3}{8}$.475	3	30.416	$6\frac{3}{4}$	154.012
$\frac{7}{16}$.647	$3\frac{1}{8}$	33.010	7	165.632
$\frac{1}{2}$.845	$3\frac{1}{4}$	35.704	$7\frac{1}{4}$	177.672
$\frac{9}{16}$	1.069	$3\frac{3}{8}$	38.503	$7\frac{1}{2}$	190.136
$\frac{5}{8}$	1.320	$3\frac{1}{2}$	41.408	$7\frac{3}{4}$	203.024
$\frac{11}{16}$	1.597	$3\frac{5}{8}$	44.418	8	216.336
$\frac{3}{4}$	1.901	$3\frac{3}{4}$	47.534	$8\frac{1}{4}$	230.068
$1\frac{1}{16}$	2.231	$3\frac{7}{8}$	50.756	$8\frac{1}{2}$	244.220
$\frac{7}{8}$	2.588	4	54.084	$8\frac{3}{4}$	258.800
$1\frac{5}{16}$	2.971	$4\frac{1}{8}$	57.517	9	273.792
1	3.380	$4\frac{1}{4}$	61.055	$9\frac{1}{4}$	289.220
$1\frac{1}{8}$	3.816	$4\frac{3}{8}$	64.700	$9\frac{1}{2}$	305.056
$1\frac{1}{4}$	4.278	$4\frac{1}{2}$	68.448	$9\frac{3}{4}$	321.332
$1\frac{3}{8}$	5.280	$4\frac{5}{8}$	72.305	10	337.920
$1\frac{1}{2}$	6.390	$4\frac{3}{4}$	76.264	$10\frac{1}{4}$	355.136
$1\frac{5}{8}$	7.604	$4\frac{7}{8}$	80.333	$10\frac{1}{2}$	372.672
$1\frac{3}{4}$	8.926	5	84.480	$10\frac{3}{4}$	390.628
$1\frac{7}{8}$	10.352	$5\frac{1}{8}$	88.784	11	408.960
2	11.883	$5\frac{1}{4}$	93.168	$11\frac{1}{4}$	427.812
$2\frac{1}{8}$	13.520	$5\frac{3}{8}$	97.657	$11\frac{1}{2}$	447.024
$2\frac{1}{4}$	15.263	$5\frac{1}{2}$	102.240	$11\frac{3}{4}$	466.684
$2\frac{3}{4}$	17.112	$5\frac{5}{8}$	106.953	12	486.656

Weight of Flat Rolled Iron, one Foot in Length.

Width.	Thickness.				
	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$
$\frac{1}{8}$.422	.528	.634	.738	.845
$\frac{1}{4}$.528	.660	.792	.923	1.056
$\frac{3}{8}$.633	.792	.950	1.108	1.265
$\frac{1}{2}$.738	.923	1.108	1.294	1.477
$\frac{5}{8}$.845	1.056	1.267	1.478	1.690
1	.950	1.187	1.425	1.663	1.901
$1\frac{1}{8}$	1.056	1.320	1.584	1.848	2.112
$1\frac{1}{4}$	1.161	1.452	1.742	2.032	2.325
$1\frac{3}{8}$	1.266	1.584	1.900	2.217	2.535
$1\frac{1}{2}$	1.372	1.716	2.059	2.402	2.746
$1\frac{5}{8}$	1.479	1.848	2.218	2.589	2.957
$1\frac{3}{4}$	1.584	1.980	2.376	2.772	3.168
2	1.689	2.112	2.534	2.957	3.379
$2\frac{1}{8}$	1.795	2.244	2.693	3.141	3.591
$2\frac{1}{4}$	1.900	2.376	2.851	3.326	3.802
$2\frac{3}{8}$	2.006	2.508	3.009	3.511	4.013
$2\frac{1}{2}$	2.112	2.640	3.168	3.696	4.224
$2\frac{5}{8}$	2.323	2.904	3.485	4.066	4.647
3	2.535	3.168	3.802	4.435	5.069
$3\frac{1}{4}$	2.746	3.432	4.119	4.805	5.492
$3\frac{1}{2}$	2.957	3.696	4.436	5.175	5.914
$3\frac{3}{4}$	3.168	3.960	4.752	5.544	6.336
4	3.380	4.224	5.069	5.914	6.759
$4\frac{1}{2}$	3.802	4.752	5.703	6.653	7.604
5	4.224	5.280	6.336	7.392	8.449
$5\frac{1}{2}$	4.647	5.808	6.970	8.132	9.294
6	5.070	6.337	7.604	8.871	10.138

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Weight of Flat Rolled Iron, one Foot in Length.

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NORWAY AND SWEDES IRON, RODS AND SHAPES,
No. 36 India Street,
Boston, Mass.

Width.	Thickness.				
	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	1	$1\frac{1}{4}$
$\frac{1}{8}$	1.056	1.265	1.477	1.690	2.112
$\frac{1}{4}$	1.320	1.584	1.846	2.112	2.640
$\frac{3}{8}$	1.584	1.901	2.217	2.534	3.168
$\frac{1}{2}$	1.846	2.217	2.588	2.956	3.696
$\frac{5}{8}$	2.112	2.534	2.956	3.380	4.224
$\frac{3}{4}$	2.375	2.850	3.326	3.802	4.752
$\frac{7}{8}$	2.640	3.168	3.696	4.224	5.280
1	2.904	3.484	4.065	4.646	5.808
$1\frac{1}{8}$	3.168	3.802	4.435	5.069	6.337
$1\frac{1}{4}$	3.432	4.119	4.805	5.492	6.864
$1\frac{3}{8}$	3.696	4.435	5.178	5.914	7.393
$1\frac{1}{2}$	3.960	4.752	5.544	6.336	7.921
$1\frac{3}{4}$	4.224	5.069	5.914	6.758	8.448
$1\frac{7}{8}$	4.488	5.386	6.283	7.181	8.977
2	4.752	5.703	6.653	7.604	9.505
$2\frac{1}{8}$	5.016	6.019	7.022	8.025	10.032
$2\frac{1}{4}$	5.280	6.336	7.392	8.448	10.560
$2\frac{3}{8}$	5.544	6.653	7.762	8.871	11.088
$2\frac{1}{2}$	5.808	6.970	8.132	9.294	11.617
$2\frac{3}{4}$	6.072	7.287	8.503	9.717	12.144
3	6.337	7.604	8.871	10.138	12.673
$3\frac{1}{8}$	6.601	7.921	9.242	10.561	13.200
$3\frac{1}{4}$	6.865	8.237	9.610	10.983	13.730
$3\frac{3}{8}$	7.129	8.554	9.979	11.406	14.259
$3\frac{1}{2}$	7.393	8.871	10.350	11.828	14.785
$3\frac{3}{4}$	7.657	9.188	10.721	12.250	15.312
4	7.921	9.505	11.089	12.673	15.841
$4\frac{1}{8}$	8.185	9.822	11.458	13.095	16.368
$4\frac{1}{4}$	8.448	10.138	11.828	13.518	16.897
$4\frac{3}{8}$	8.712	10.455	12.197	13.940	17.424
$4\frac{1}{2}$	8.976	10.771	12.567	14.363	17.952
$4\frac{3}{4}$	9.240	11.088	12.937	14.785	18.479
5	9.504	11.406	13.306	15.208	19.008
$5\frac{1}{8}$	9.768	11.722	13.676	15.630	19.536
$5\frac{1}{4}$	10.032	12.039	14.045	16.053	20.064
$5\frac{3}{8}$	10.296	12.356	14.415	16.475	20.592
$5\frac{1}{2}$	10.560	12.673	14.784	16.897	21.120
$5\frac{3}{4}$	10.824	12.989	15.154	17.320	21.648
6	11.088	13.306	15.523	17.742	22.176
$6\frac{1}{8}$	11.352	13.623	15.893	18.165	22.704
$6\frac{1}{4}$	11.616	13.940	16.264	18.587	23.232
$6\frac{3}{8}$	11.880	14.257	16.634	19.010	23.760
$6\frac{1}{2}$	12.144	14.574	17.004	19.432	24.288
$6\frac{3}{4}$	12.408	14.891	17.374	19.855	24.816
7	12.672	15.208	17.744	20.277	25.344

Weight of Wrought Angle Iron, one Foot in Length,
Thickness Measured in the Middle of each Side.

EQUAL SIDES.		
Sides.	Thickness.	Weight.
Inches.	Inches.	Pounds.
1.25 × 1.25	$\frac{3}{16}$	1.5
1.5 × 1.5	$\frac{3}{16}$	2.
1.75 × 1.75	$\frac{1}{4}$	3.
2. × 2.	$\frac{1}{4}$	3.5
2.25 × 2.25	$\frac{5}{16}$	4.5
2.5 × 2.5	$\frac{5}{16}$	5.
3. × 3.	$\frac{3}{8}$	7.
3.5 × 3.5	$\frac{7}{16}$	9.
4. × 4.	$\frac{1}{2}$	12.5
4.5 × 4.5	$\frac{1}{2}$	14.
4.5 × 4.5	$\frac{9}{16}$	16.
UNEQUAL SIDES.		
3.5 × 3.	$\frac{7}{16}$	9.6
4. × 3.	$\frac{1}{2}$	11.
4. × 3.5	$\frac{1}{2}$	11.5
4. × 3.5	$\frac{9}{16}$	11.75
4.5 × 3.	$\frac{9}{16}$	11.75
5. × 3.	$\frac{1}{2}$	12.65
5. × 3.	$\frac{9}{16}$	13.7
5.5 × 3.5	$\frac{1}{2}$	14.5
5.5 × 3.5	$\frac{9}{16}$	15.6
6. × 3.5	$\frac{5}{8}$	18.
6. × 4.5	$\frac{5}{8}$	20.

HENRY M. JOHNSON,
BAR, HOOP, SHEET, AND ANGLE IRON,
No. 36 India Street,
Boston, Mass.

Whale or Oil Cask Hoops.

HENRY M. JOHNSON,
NORWAY AND SWEDES IRON, RODS AND SHAPES,
Boston, Mass
No. 36 India Street.

Weight.	Penny.	Width.	W. G.	W't. pr Ft.
Light	3d.	1½	14	.3122
Heavy	3d.	1½	13	.3574
Light	4d.	1¼	13	.3971
Heavy	4d.	1¾	12	.5011
Light	5d.	1½	11	.6019
Heavy	5d.	1¾	10	.7281
Light	6d.	1¾	10	.7841
Heavy	6d.	1¾	9	.8660

Table of the Thickness and Weight
of Galvanized Sheet Iron.

Dimensions of Sheet, 2 to 3 Feet in Width by
from 6 to 9 Feet in Length.

Wire Gauge.		W'ght per Sq. Foot.	
Number.	Ounces.	Number.	Ounces.
30	10	22	21
29	11	21	24
28	12	20	28
27	14	19	33
26	15	18	37
25	16	17	43
24	17	16	48
23	19	14	60

Weight of Hoop and Band Iron, one Foot in
Length — Birmingham Wire Gauge.

	W. G.	W. G.	W. G.	W. G.	W. G.
Width.	22	21	20	19	18
$\frac{1}{2}$.0468	.0535	.0585	.0702	.0819
$\frac{5}{8}$.0585	.0668	.0731	.0877	.1024
$\frac{3}{4}$.0702	.0802	.0878	.1053	.1229
$\frac{7}{8}$.0819	.0936	.1024	.1228	.1434
1	.0936	.1070	.1170	.1404	.1638
$1\frac{1}{8}$.1053	.1204	.1316	.1579	.1843
$1\frac{1}{4}$.1170	.1337	.1463	.1755	.2048
$1\frac{3}{8}$.1287	.1471	.1609	.1930	.2253
$1\frac{1}{2}$.1404	.1605	.1755	.2106	.2458
$1\frac{5}{8}$.1521	.1739	.1901	.2281	.2663
$1\frac{3}{4}$.1638	.1872	.2048	.2457	.2867
$1\frac{7}{8}$.1755	.2006	.2194	.2632	.3072
2	.1872	.2140	.2341	.2808	.3276
$2\frac{1}{4}$.2106	.2407	.2633	.3159	.3686
$2\frac{1}{2}$.2340	.2675	.2926	.3510	.4096
$2\frac{3}{4}$.2574	.2942	.3219	.3861	.4506
3	.2808	.3210	.3510	.4212	.4914

HENRY M. JOHNSON,
BAR, HOOP, SHEET, AND ANGLE IRON,
No. 36 India Street,
Boston, Mass.

Weight of Hoop and Band Iron, one Foot in
Length — Birmingham Wire Gauge.

HENRY M. JOHNSON,
NORWAY AND SWEDES IRON, RODS AND SHAPES,
Boston, Mass.
No. 36 India Street,

Width.	W. G.	W. G.	W. G.	W. G.	W. G.
	17	16	15	14	13
$\frac{1}{2}$.0970	.1087	.1204	.1388	.1588
$\frac{5}{8}$.1212	.1359	.1505	.1735	.1985
$\frac{3}{4}$.1455	.1630	.1806	.2081	.2382
$\frac{7}{8}$.1697	.1902	.2107	.2428	.2779
1	.1939	.2173	.2407	.2775	.3177
$1\frac{1}{8}$.2182	.2445	.2708	.3122	.3574
$1\frac{1}{4}$.2424	.2717	.3009	.3469	.3971
$1\frac{3}{8}$.2667	.2988	.3310	.3816	.4368
$1\frac{1}{2}$.2909	.3260	.3611	.4163	.4765
$1\frac{5}{8}$.3151	.3532	.3912	.4510	.5162
$1\frac{3}{4}$.3394	.3803	.4213	.4857	.5559
$1\frac{7}{8}$.3636	.4075	.4514	.5204	.5956
2	.3879	.4347	.4815	.5551	.6353
$2\frac{1}{4}$.4364	.4890	.5417	.6245	.7147
$2\frac{1}{2}$.4849	.5434	.6019	.6939	.7941
$2\frac{3}{4}$.5334	.5977	.6621	.7632	.8735
3	.5818	.6520	.7222	.8326	.9530

Weight of Hoop and Band Iron, one Foot in
Length — Birmingham Wire Gauge.

	W. G.	W. G.	W. G.	W. G.	W. G.
Width.	12	11	10	9	8
$\frac{1}{2}$.1822	.2006	.2240	.2474	.2759
$\frac{5}{8}$.2278	.2507	.2800	.3093	.3418
$\frac{3}{4}$.2733	.3009	.3360	.3711	.4138
$\frac{7}{8}$.3189	.3511	.3920	.4330	.4828
1	.3645	.4012	.4480	.4940	.5517
$1\frac{1}{8}$.4100	.4514	.5040	.5568	.6207
$1\frac{1}{4}$.4556	.5015	.5600	.6186	.6896
$1\frac{3}{8}$.5011	.5517	.6160	.6805	.7586
$1\frac{1}{2}$.5467	.6019	.6721	.7423	.8276
$1\frac{5}{8}$.5922	.6520	.7281	.8042	.8966
$1\frac{3}{4}$.6378	.7022	.7841	.8660	.9655
$1\frac{7}{8}$.6834	.7523	.8401	.9279	1.0341
2	.7289	.8025	.8961	.9897	1.1034
$2\frac{1}{4}$.8200	.9028	1.0081	1.1134	1.2413
$2\frac{1}{2}$.9111	1.0031	1.1201	1.2371	1.3793
$2\frac{3}{4}$	1.0022	1.1034	1.2321	1.3608	1.5172
3	1.0934	1.2037	1.3442	1.4846	1.6551

HENRY M. JOHNSON,
BAR, HOOP, SHEET, AND ANGLE IRON,
No. 36 India Street,
Boston, Mass.

Weight of Hoop and Band Iron, one Foot in
Length — Birmingham Wire Gauge.

HENRY M. JOHNSON,
NORWAY AND SWEDES IRON, RODS AND SHAPES,
Boston, Mass.
No. 36 India Street,

Width.	W. G.	W. G.	W. G.	W. G.	W. G.
	7	6	5	4	3
$\frac{1}{2}$.3010	.3394	.3678	.3978	.4330
$\frac{5}{8}$.3762	.4242	.4597	.4973	.5412
$\frac{3}{4}$.4514	.5091	.5517	.5968	.6495
$\frac{7}{8}$.5267	.5939	.6436	.6963	.7577
1	.6020	.6788	.7356	.7958	.8660
$1\frac{1}{8}$.6772	.7636	.8275	.8952	.9743
$1\frac{1}{4}$.7525	.8485	.9195	.9947	1.0825
$1\frac{3}{8}$.8277	.9333	1.0114	1.0942	1.1908
$1\frac{1}{2}$.9028	1.0182	1.1034	1.1937	1.2990
$1\frac{5}{8}$.9780	1.1030	1.1953	1.2932	1.4072
$1\frac{3}{4}$	1.0533	1.1879	1.2873	1.3926	1.5155
$1\frac{7}{8}$	1.1285	1.2727	1.3792	1.4922	1.6237
2	1.2037	1.3576	1.4712	1.5916	1.7321
$2\frac{1}{4}$	1.3542	1.5274	1.6551	1.7905	1.9486
$2\frac{1}{2}$	1.5047	1.6970	1.8390	1.9894	2.1651
$2\frac{3}{4}$	1.6551	1.8667	2.0229	2.1884	2.3816
3	1.8056	2.0363	2.2069	2.3874	2.5981

Weights of Wrought Iron and Steel.

Thickness determined by Birmingham Gauge.

No. of Gauge.	Thickness of each No.	Plates — per Sq. Foot.	
		Iron.	Steel.
	Inches.	Pounds.	Pounds.
0000	.454	18.2167	18.4596
000	.425	17.0531	17.2805
00	.38	15.2475	15.4508
0	.34	13.6425	13.8244
1	.3	12.0375	12.198
2	.284	11.3955	11.5474
3	.259	10.3924	10.5309
4	.238	9.5497	9.6771
5	.22	8.8275	8.9452
6	.203	8.1454	8.254
7	.18	7.2225	7.3188
8	.165	6.6206	6.7089
9	.148	5.9385	6.0177
10	.134	5.3767	5.4484
11	.12	4.815	4.8792
12	.109	4.3736	4.4319
13	.095	3.8119	3.8627
14	.083	3.3304	3.3748
15	.072	2.889	2.9275
16	.065	2.6081	2.6429
17	.058	2.3272	2.3583
18	.049	1.9661	1.9923

HENRY M. JOHNSON,
 BAR, HOOP, SHEET, AND ANGLE IRON,
 No. 36 India Street,
 Boston, Mass.

Weights of Wrought Iron and Steel.

Thickness determined by Birmingham Gauge.

HENRY M. JOHNSON, NORWAY AND SWEDES IRON, RODS AND SHAPES, No. 36 India Street, Boston, Mass.	No. of Gauge.	Thickness of each No.	Plates — per Sq. Foot.	
			Iron.	Steel.
		Inches.	Pounds.	Pounds.
	19	.042	1.6852	1.7077
	20	.035	1.4044	1.4231
	21	.032	1.284	1.3011
	22	.028	1.1235	1.1385
	23	.025	1.0031	1.0165
	24	.022	.8827	.8945
	25	.02	.8025	.8132
	26	.018	.7222	.7319
	27	.016	.642	.6506
	28	.014	.5617	.5692
	29	.013	.5216	.5286
	30	.012	.4815	.4879
	31	.01	.4012	.4066
	32	.009	.3611	.3659
	33	.008	.321	.3253
	34	.007	.2809	.2846
	35	.005	.2006	.2033
	36	.004	.1605	.1626

24 WEIGHTS OF COPPER AND BRASS.

Weights of Copper and Brass Plates.

Thickness determined by Birmingham Gauge.

No. of Gauge.	Thickness of each No.	Plates — per Sq. Foot.	
		Copper.	Brass.
	Inches.	Pounds.	Pounds.
0000	.454	20.5662	19.4312
000	.425	19.2525	18.19
00	.38	17.214	16.264
0	.34	15.402	14.552
1	.3	13.59	12.84
2	.284	12.8652	12.1552
3	.259	11.7327	11.0852
4	.238	10.7814	10.1864
5	.22	9.966	9.416
6	.203	9.1959	8.6884
7	.18	8.154	7.704
8	.165	7.4745	7.062
9	.148	6.7044	6.3344
10	.134	6.0702	5.7352
11	.12	5.436	5.136
12	.109	4.9377	4.6652
13	.095	4.3035	4.066
14	.083	3.7599	3.5524
15	.072	3.2616	3.0816
16	.065	2.9445	2.782
17	.058	2.6274	2.4824
18	.049	2.2197	2.0972

HENRY M. JOHNSON,
 BAR, HOOP, SHEET, AND ANGLE IRON,
 No. 36 India Street,
 Boston, Mass.

Weights of Copper and Brass Plates.

Thickness determined by Birmingham Gauge.

HENRY M. JOHNSON, NORWAY AND SWEDES IRON, RODS AND SHAPES, Boston, Mass. No. 36 India Street,	No. of Gauge.	Thickness of each No.	Plates — per Sq. Foot.	
			Copper.	Brass.
		Inches.	Pounds.	Pounds.
	19	.042	1.9026	1.7976
	20	.035	1.5855	1.498
	21	.032	1.4496	1.3696
	22	.028	1.2684	1.1984
	23	.025	1.1325	1.07
	24	.022	.9966	.9413
	25	.02	.906	.856
	26	.018	.8154	.7704
	27	.016	.7248	.6848
	28	.014	.6342	.5992
	29	.013	.5889	.5564
	30	.012	.5436	.5136
	31	.01	.453	.428
	32	.009	.4077	.382
	33	.008	.3624	.3424
	34	.007	.3171	.2996
	35	.005	.2265	.214
	36	.004	.1812	.1712

TIN PLATES.

Mark.	Number of Sheets per Box.	Length and Breadth in Inches.	W'ght per Box.
IC	225	10 X 14	112
IX	225	10 X 14	140
IXX	225	10 X 14	161
IXXX	225	10 X 14	182
IXXXX	225	10 X 14	203
IC	112	14 X 20	112
IX	112	14 X 20	140
IXX	112	14 X 20	168
IXXX	112	14 X 20	196
IXXXX	112	14 X 20	224
DC	100	12½ X 17	98
DX	100	12½ X 17	126
DXX	100	12½ X 17	147
DXXX	100	12½ X 17	168
DXXXX	100	12½ X 17	189
SDC	200	11 X 15	167
SDX	200	11 X 15	188
SDXX	200	11 X 15	209
SDXXX	200	11 X 15	230
SDXXXX	200	11 X 15	251
IIC	225	9¾ X 13¼	105
IIX	225	9¾ X 13¼	133
IIIC	225	9½ X 12¾	98

HENRY M. JOHNSON,
 BAR, HOOP, SHEET, AND ANGLE IRON,
 No. 36 India Street,
 Boston, Mass.

TABLE — Continued.

HENRY M. JOHNSON, NORWAY AND SWEDES IRON, RODS AND SHAPES, Boston, Mass. No. 36 India Street,	Mark.	Number of Sheets per Box.	Length and Breadth in Inches.	Weight per Box.
	IIIX . . .	225	9½ × 12¾	126
	TT	450	10 × 14	112
	XTT . . .	450	10 × 14	126
	IC	225	11 × 11	96
	IC	225	13 × 13	140
	IC	225	14 × 14	168 ^{3/4}
	IXX . . .	These sizes are sold at — per lb.	12 × 24	28 - 1.5
	IXXX . .		13 × 21	
	IXXXX .		14 × 22	
	IXXXXX		14 × 26	
	IXXXXXX		14 × 26½	
	IC	225	12 × 12	115
	IX	225	12 × 12	144
	IXX . . .	225	12 × 12	166
	IXXX . .	225	12 × 12	187
	IXXXX .	225	12 × 12	209
— ♦ —				
TERNE PLATES.				
	IC	112	14 × 20	112
	IX	112	14 × 20	140

Weight of Cast Iron Pipes of different Thicknesses,
From 1 Inch to 36 Inches in Diameter.

One Foot in Length.

Diam.	Thick.	W'ght.	Diam.	Thick.	W'ght.
Inches.	Inches.	Pounds.	Inches.	Inches.	Pounds.
1.	$\frac{1}{4}$	3.06	3. $\frac{3}{4}$	$\frac{1}{2}$	20.9
1.	$\frac{3}{8}$	5.05	3. $\frac{3}{4}$	$\frac{5}{8}$	26.83
1. $\frac{1}{4}$	$\frac{1}{4}$	3.67	3. $\frac{3}{4}$	$\frac{3}{4}$	33.07
1. $\frac{1}{4}$	$\frac{3}{8}$	6.	4.	$\frac{1}{2}$	22.05
1. $\frac{1}{2}$	$\frac{3}{8}$	6.89	4.	$\frac{5}{8}$	28.28
1. $\frac{1}{2}$	$\frac{1}{2}$	9.8	4.	$\frac{3}{4}$	34.94
1. $\frac{3}{4}$	$\frac{3}{8}$	7.8	4. $\frac{1}{4}$	$\frac{1}{2}$	23.35
1. $\frac{3}{4}$	$\frac{1}{2}$	11.04	4. $\frac{1}{4}$	$\frac{5}{8}$	29.85
2.	$\frac{3}{8}$	8.74	4. $\frac{1}{4}$	$\frac{3}{4}$	36.73
2.	$\frac{1}{2}$	12.23	4. $\frac{1}{2}$	$\frac{1}{2}$	24.49
2. $\frac{1}{4}$	$\frac{3}{8}$	9.65	4. $\frac{1}{2}$	$\frac{5}{8}$	31.4
2. $\frac{1}{4}$	$\frac{1}{2}$	13.48	4. $\frac{1}{2}$	$\frac{3}{4}$	38.58
2. $\frac{1}{2}$	$\frac{3}{8}$	10.57	4. $\frac{3}{4}$	$\frac{1}{2}$	25.7
2. $\frac{1}{2}$	$\frac{1}{2}$	14.66	4. $\frac{3}{4}$	$\frac{5}{8}$	32.91
2. $\frac{1}{2}$	$\frac{5}{8}$	19.05	4. $\frac{3}{4}$	$\frac{3}{4}$	40.43
2. $\frac{3}{4}$	$\frac{3}{8}$	11.54	5.	$\frac{1}{2}$	26.94
2. $\frac{3}{4}$	$\frac{1}{2}$	15.91	5.	$\frac{5}{8}$	34.34
2. $\frac{3}{4}$	$\frac{5}{8}$	20.59	5.	$\frac{3}{4}$	42.28
3.	$\frac{3}{8}$	12.28	5. $\frac{1}{2}$	$\frac{1}{2}$	29.4
3.	$\frac{1}{2}$	17.15	5. $\frac{1}{2}$	$\frac{5}{8}$	37.44
3.	$\frac{5}{8}$	22.15	5. $\frac{1}{2}$	$\frac{3}{4}$	45.94
3.	$\frac{3}{4}$	27.56	6.	$\frac{1}{2}$	31.82
3. $\frac{1}{4}$	$\frac{1}{2}$	18.4	6.	$\frac{5}{8}$	40.56
3. $\frac{1}{4}$	$\frac{5}{8}$	23.72	6.	$\frac{3}{4}$	49.6
3. $\frac{1}{4}$	$\frac{3}{4}$	29.64	6.	$\frac{7}{8}$	58.96
3. $\frac{1}{2}$	$\frac{1}{2}$	19.66	6. $\frac{1}{2}$	$\frac{1}{2}$	34.32
3. $\frac{1}{2}$	$\frac{5}{8}$	25.27	6. $\frac{1}{2}$	$\frac{5}{8}$	43.68
3. $\frac{1}{2}$	$\frac{3}{4}$	31.2	6. $\frac{1}{2}$	$\frac{3}{4}$	53.3

HENRY M. JOHNSON,
BAR, HOOP, SHEET, AND ANGLE IRON,
No. 36 India Street,
Boston, Mass.

TABLE—Continued.

	Diam.	Thick.	W'ght.	Diam.	Thick.	W'ght.
	Inches.	Inches.	Pounds.	Inches.	Inches.	Pounds.
HENRY M. JOHNSON, NORWAY AND SWEDES IRON, RODS AND SHAPES, Boston, Mass. No. 36 India Street,	6.½	.⅞	63.18	9.½	1.	102.9
	7.	.½	36.66	10.	.½	51.46
	7.	.⅝	46.8	10.	.⅝	65.08
	7.	.¾	56.96	10.	.¾	78.99
	7.	.⅞	67.6	10.	.⅞	93.24
	7.	1.	78.39	10.	1.	108.84
	7.½	.½	39.22	10.½	.½	53.88
	7.½	.⅝	49.92	10.½	.⅝	68.14
	7.½	.¾	60.48	10.½	.¾	82.68
	7.½	.⅞	71.76	10.½	.⅞	97.44
	7.½	1.	83.28	10.½	1.	112.68
	8.	.½	41.64	11.	.½	56.34
	8.	.⅝	52.68	11.	.⅝	71.19
	8.	.¾	64.27	11.	.¾	86.4
	8.	.⅞	76.12	11.	.⅞	101.83
	8.	1.	88.2	11.	1.	117.6
	8.½	.½	44.11	11.½	.½	58.82
	8.½	.⅝	56.16	11.½	.⅝	74.28
	8.½	.¾	68.	11.½	.¾	90.06
	8.½	.⅞	80.5	11.½	.⅞	106.14
	8.½	1.	93.28	11.½	1.	122.62
	9.	.½	46.5	12.	.½	61.26
	9.	.⅝	58.92	12.	.⅝	77.36
	9.	.¾	71.7	12.	.¾	93.7
	9.	.⅞	84.7	12.	.⅞	110.48
	9.	1.	97.98	12.	1.	127.42
	9.½	.½	48.98	12.½	.½	63.7
	9.½	.⅝	62.02	12.½	.⅝	80.4
	9.½	.¾	75.32	12.½	.¾	97.4
	9.½	.⅞	88.98	12.½	.⅞	114.72

TABLE—Continued.

Diam.	Thick.	W'ght.	Diam.	Thick.	W'ght.
Inches.	Inches.	Pounds.	Inches.	Inches.	Pounds.
12.½	1.	132.35	15.½	1.	161.82
13.	½	66.14	16.	½	80.87
13.	⅝	83.46	16.	⅝	101.82
13.	¾	101.08	16.	¾	123.14
13.	⅞	118.97	16.	⅞	144.76
13.	1.	137.28	16.	1.	166.6
13.½	½	68.36	17.	½	85.73
13.½	⅝	86.55	17.	⅝	107.96
13.½	¾	104.76	17.	¾	130.48
13.½	⅞	123.3	17.	⅞	153.3
13.½	1.	142.16	17.	1.	176.58
14.	½	71.07	18.	½	114.1
14.	⅝	89.61	18.	⅝	137.84
14.	¾	108.46	18.	¾	161.9
14.	⅞	127.6	18.	⅞	186.24
14.	1.	147.03	19.	1.	205.8
14.½	½	73.72	19.	½	120.24
14.½	⅝	92.66	19.	⅝	145.2
14.½	¾	112.1	19.	¾	170.47
14.½	⅞	131.86	19.	⅞	195.92
14.½	1.	151.92	20.	1.	226.33
15.	½	75.96	20.	½	152.53
15.	⅝	95.72	20.	⅝	179.02
15.	¾	115.78	20.	¾	205.8
15.	⅞	136.15	21.	⅞	132.5
15.	1.	156.82	21.	1.	159.84
15.½	½	78.4	21.	½	187.6
15.½	⅝	98.78	21.	⅝	215.52
15.½	¾	119.48	22.	¾	138.6
15.½	⅞	140.4	22.	⅞	167.24
			22.	1.	196.46

HENRY M. JOHNSON,
 BAR, HOOP, SHEET, AND ANGLE IRON,
 No. 36 India Street,
 Boston, Mass.

TABLE—Continued.

HENRY M. JOHNSON, NORWAY AND SWEDES IRON, RODS AND SHAPES, Boston, Mass. No. 36 India Street,	Diam.	Thick.	W'ght.	Diam.	Thick.	W'ght
	Inches.	Inches.	Pounds.	Inches.	Inches.	Pounds.
22.	1.		225.38	31.	$\frac{3}{4}$	233.4
23.	$\frac{5}{8}$		144.77	31.	$\frac{7}{8}$	273.4
23.	$\frac{3}{4}$		174.62	31.	1.	313.68
23.	$\frac{7}{8}$		204.78	31.	$1\frac{1}{8}$	354.24
23.	1.		235.28	32.	$\frac{3}{4}$	240.76
24.	$\frac{5}{8}$		150.85	32.	$\frac{7}{8}$	281.94
24.	$\frac{3}{4}$		181.92	32.	1.	323.49
24.	$\frac{7}{8}$		213.28	32.	$1\frac{1}{8}$	365.29
24.	1.		245.08	33.	$\frac{3}{4}$	248.1
25.	$\frac{5}{8}$		156.97	33.	$\frac{7}{8}$	290.5
25.	$\frac{3}{4}$		189.28	33.	1.	333.24
25.	$\frac{7}{8}$		221.94	33.	$1\frac{1}{8}$	376.26
25.	1.		254.86	33.	$1\frac{1}{4}$	420.77
26.	$\frac{3}{4}$		196.62	34.	$\frac{3}{4}$	255.45
26.	$\frac{7}{8}$		230.56	34.	$\frac{7}{8}$	298.88
26.	1.		264.66	34.	1.	342.88
27.	$\frac{3}{4}$		204.04	34.	$1\frac{1}{8}$	387.13
27.	$\frac{7}{8}$		239.08	34.	$1\frac{1}{4}$	431.76
27.	1.		274.56	35.	$\frac{3}{4}$	262.7
28.	$\frac{3}{4}$		211.32	35.	$\frac{7}{8}$	307.62
28.	$\frac{7}{8}$		247.62	35.	1.	352.86
28.	1.		284.28	35.	$1\frac{1}{8}$	398.1
29.	$\frac{3}{4}$		218.7	35.	$1\frac{1}{4}$	443.96
29.	$\frac{7}{8}$		256.2	36.	$\frac{3}{4}$	270.18
29.	1.		294.02	36.	$\frac{7}{8}$	316.36
30.	$\frac{3}{4}$		226.2	36.	1.	362.86
30.	$\frac{7}{8}$		264.79	36.	$1\frac{1}{8}$	409.34
30.	1.		303.86	36.	$1\frac{1}{4}$	456.46
30.	$1\frac{1}{8}$		343.2			

NOTE.—These weights do not include any allowance for spigot and faucet ends.

Table of Standard Dimensions of Wrought Iron
Welded Tubes.

Nominal Diam.	External Diam	Thickness.	Internal Diam.	Internal Circumf.	External Circumf.
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
$\frac{1}{8}$.40	.068	.27	.85	1.27
$\frac{1}{4}$.54	.088	.36	1.14	1.7
$\frac{3}{8}$.67	.091	.49	1.55	2.12
$\frac{1}{2}$.84	.109	.62	1.96	2.65
$\frac{3}{4}$	1.05	.113	.82	2.59	3.3
1	1.31	.134	1.05	3.29	4.13
$1\frac{1}{4}$	1.66	.14	1.38	4.33	5.21
$1\frac{1}{2}$	1.9	.145	1.61	5.06	5.97
2	2.37	.154	2.07	6.49	7.46
$2\frac{1}{2}$	2.87	.204	2.47	7.75	9.03
3	3.5	.217	3.07	9.64	11.
$3\frac{1}{2}$	4.	.226	3.55	11.15	12.57
4	4.5	.237	4.07	12.69	14.14
$4\frac{1}{2}$	5.	.247	4.51	14.15	15.71
5	5.56	.259	5.04	15.85	17.47
6	6.62	.28	6.06	19.05	20.81
7	7.62	.301	7.02	22.06	23.95
8	8.62	.322	7.98	25.08	27.1
9	9.69	.344	9.	28.28	30.43
10	10.75	.366	10.02	31.47	33.77

HENRY M. JOHNSON,
 BAR, HOOP, SHEET, AND ANGLE IRON,
 No. 36 India Street,
 Boston, Mass.

Table of Standard Dimensions of Wrought Iron
Welded Tubes.

HENRY M. JOHNSON, NORWAY AND SWEDES IRON, RODS AND SHAPES, Boston, Mass.		Nominal Diam.	L'gth of Pipe per Sq. Ft. of Inter- nal Surface.	L'gth of Pipe per Sq. Ft. of Exter- nal Surface.	Internal Area.	Weight per Foot.	No. of Threads per In. of Screw.
		Inches.	Feet..	Feet.	Inches.	Pounds.	
		$\frac{1}{8}$	14.15	9.44	.057	.24	27
		$\frac{1}{4}$	10.5	7.075	.104	.42	18
		$\frac{3}{8}$	7.67	5.657	.192	.56	18
		$\frac{1}{2}$	6.13	4.502	.305	.84	14
		$\frac{3}{4}$	4.64	3.637	.533	1.13	14
		1	3.66	2.903	.863	1.67	11½
		1¼	2.77	2.301	1.496	2.26	11½
		1½	2.37	2.01	2.038	2.69	11½
		2	1.85	1.611	3.355	3.67	11½
		2½	1.55	1.328	4.783	5.77	8
		3	1.24	1.091	7.388	7.55	8
		3½	1.08	0.955	9.887	9.05	8
		4	.95	0.849	12.73	10.73	8
		4½	.85	0.765	15.939	12.49	8
		5	.78	0.629	19.99	14.56	8
		6	.63	0.577	28.889	18.77	8
		7	.54	0.505	38.737	23.41	8
		8	.48	0.444	50.039	28.35	8
		9	.42	0.394	63.633	34.08	8
		10	.38	0.355	78.838	40.64	8

34 LENGTH OF HORSESHOE NAILS, ETC.

Weight of Composition Sheathing Nails.

No.	L'gth.	No. in a Pound.	No.	L'gth.	No. in a Pound.
	Inches.			Inches.	
1	$\frac{3}{4}$	290	8	$1\frac{1}{4}$	168
2	$\frac{7}{8}$	260	9	$1\frac{1}{2}$	110
3	1	212	10	$1\frac{3}{8}$	101
4	$1\frac{1}{8}$	201	11	$1\frac{3}{4}$	74
5	$1\frac{1}{4}$	199	12	2	64
6	1	190	13	$2\frac{1}{4}$	59
7	$1\frac{1}{8}$	184			

Length of Horseshoe Nails.

No. 5 . . $1\frac{1}{2}$	Ins.	No. 8 . . 2	Ins.
" 6 . . $1\frac{3}{4}$	"	" 9 . . $2\frac{1}{4}$	"
" 7 . . $1\frac{7}{8}$	"	" 10 . . $2\frac{1}{2}$	"

L'gths of Iron Nails, and No. in Pound.

Size.	Length.	No.	Size.	Length.	No.
3d.	$1\frac{1}{4}$	427	10d.	3	61
4	$1\frac{1}{2}$	264	12	$3\frac{1}{4}$	50
5	$1\frac{3}{4}$	206	20	$3\frac{1}{2}$	37
6	2	146	30	4	24
8	$2\frac{1}{2}$	95	40	$4\frac{1}{4}$	17

HENRY M. JOHNSON,
 BAR, HOOP, SHEET, AND ANGLE IRON,
 No. 36 India Street,
 Boston, Mass.

Value of Iron per Ton of 2240 Pounds,

At from 2 Cents to 12 Cents per Pound.

HENRY M. JOHNSON, NORWAY AND SWEDES IRON, RODS AND SHAPES, Boston, Mass. No. 36 India Street,	2	44.80	5 $\frac{3}{8}$	120.40	8 $\frac{3}{4}$	196.00
	2 $\frac{1}{8}$	47.60	5 $\frac{1}{2}$	123.20	8 $\frac{7}{8}$	198.80
	2 $\frac{1}{4}$	50.40	5 $\frac{5}{8}$	126.00	9	201.60
	2 $\frac{3}{8}$	53.20	5 $\frac{3}{4}$	128.80	9 $\frac{1}{8}$	204.40
	2 $\frac{1}{2}$	56.00	5 $\frac{7}{8}$	131.60	9 $\frac{1}{4}$	207.20
	2 $\frac{5}{8}$	58.80	6	134.40	9 $\frac{3}{8}$	210.00
	2 $\frac{3}{4}$	61.60	6 $\frac{1}{8}$	137.20	9 $\frac{1}{2}$	212.80
	2 $\frac{7}{8}$	64.40	6 $\frac{1}{4}$	140.00	9 $\frac{5}{8}$	215.60
	3	67.20	6 $\frac{3}{8}$	142.80	9 $\frac{3}{4}$	218.40
	3 $\frac{1}{8}$	70.00	6 $\frac{1}{2}$	145.60	9 $\frac{7}{8}$	221.20
	3 $\frac{1}{4}$	72.80	6 $\frac{5}{8}$	148.40	10	224.00
	3 $\frac{3}{8}$	75.60	6 $\frac{3}{4}$	151.20	10 $\frac{1}{8}$	226.80
	3 $\frac{1}{2}$	78.40	6 $\frac{7}{8}$	154.00	10 $\frac{1}{4}$	229.60
	3 $\frac{5}{8}$	81.20	7	156.80	10 $\frac{3}{8}$	232.40
	3 $\frac{3}{4}$	84.00	7 $\frac{1}{8}$	159.60	10 $\frac{1}{2}$	235.20
	3 $\frac{7}{8}$	86.80	7 $\frac{1}{4}$	162.40	10 $\frac{5}{8}$	238.00
	4	89.60	7 $\frac{3}{8}$	165.20	10 $\frac{3}{4}$	240.80
	4 $\frac{1}{8}$	92.40	7 $\frac{1}{2}$	168.00	10 $\frac{7}{8}$	243.60
	4 $\frac{1}{4}$	95.20	7 $\frac{5}{8}$	170.80	11	246.40
	4 $\frac{3}{8}$	98.00	7 $\frac{3}{4}$	173.60	11 $\frac{1}{8}$	249.20
	4 $\frac{1}{2}$	100.80	7 $\frac{7}{8}$	176.40	11 $\frac{1}{4}$	252.00
	4 $\frac{5}{8}$	103.60	8	179.20	11 $\frac{3}{8}$	254.80
	4 $\frac{3}{4}$	106.40	8 $\frac{1}{8}$	182.00	11 $\frac{1}{2}$	257.60
	4 $\frac{7}{8}$	109.20	8 $\frac{1}{4}$	184.80	11 $\frac{5}{8}$	260.40
	5	112.00	8 $\frac{3}{8}$	187.60	11 $\frac{3}{4}$	263.20
	5 $\frac{1}{8}$	114.80	8 $\frac{1}{2}$	190.40	11 $\frac{7}{8}$	266.00
	5 $\frac{1}{4}$	117.60	8 $\frac{5}{8}$	193.20	12	268.80

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